



Quench Protection for High Field Magnets ($>12\text{T}$) (Accelerator Type)

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Conditions assumed in talk

- Protection to be accomplished by a close proximity heater
- Highly efficient coil winding package $J_{cu} > 1000$ A/ mm²
- Examples given will be limited to Nb₃Sn coils.
“Should be applicable to other A-15’s”
- Heater constructed composites of Kapton/ SS(cu)/ Kapton plus glue



Definitions

| | | |
|---|---|---|
| Conductor Miits | ≡ | $10^6 \text{ Amp}^2 \text{-sec}$ to reach 450 K a) measured b) adiabatic calculation |
| Critical ramp rate | ≡ | Rate of current change at which conductor exceeds its critical temperature of the average winding field in a 0.1 operating current loss |
| Minimum Protection Winding volume transitioning | ≡ | That length of conductor which will result in a L/ R time constant that will stay below the conductor Miits budget |



Design input needed

Conductor

- dimensions
- composition
- geometry
- critical current, field, and temperature profile

Windings

- operating current, (load line)
- geometry
- electrical parameters
- magnetic parameters

Note: Any of these can be obtained by measurement (all the better) or calculated. Operational characteristics LHe II or I, open or closed winding.

Comment: (will not consider cryostable operating point coils due to time constraints)



Typical Design of a heater for a Nb₃Sn Race Track Coil

Conductor Parameters:

26 strand cable

0.8 mm strand diameter

$J_c(\text{non-cu}) = 2000^+ \text{ amps/mm}^2$

Typical design input:

Quench output page

Typical Miits Curve:

Quench's Miit's Curve RD3

First order heater considerations RD3:

Induct. = 18mh

$L/R = ?$

at 10kA/turn yields 100 Miit's/sec

Miit's limit "Quench" = 12.4

$\Rightarrow 125 \text{ milliseconds}$

- $\frac{40}{85}$ " " detection & diffusion

$\Rightarrow 0.17 \text{ seconds} = t(\text{effective})$

$R = 0.018/0.17 \sim 0.1 \text{ ohms}$

Outer coil's room temperature resistance = 0.75 ohms

20K $R(\text{expected}) = 0.02 \text{ ohms}$

20K $R(\text{measured}) = 0.058$ "

$\Rightarrow \frac{1}{4}$ of the coil driven normal will work



“Quench” code input/output for Miit’s

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COMPONENT PROPERTIES
FRAC TESTA A AFX B BFX C CRX D DFX DRAC
.4040 .50 .4250E-07 .0000 .670E-11 .6900 .9000E-15 .6000 .0000E-00 .0000 .0000
.4080 .45.00 .4250E-07 .0000 .670E-11 .6900 .2300E-12 .1500 .0000E-00 .0000 .0000
.4090 .150.00 .380E-06 .2300 .0000E-10 .0000 .3000E+11 .0000 .1200E-03 .1.0000 .0000
.0710 .50 .1700E-05 .1200 .670E-11 .2.6900 .0000E-05 .3.0000 .0000E-00 .0000 .0000
.0710 .40.00 .1700E-05 .1200 .670E-11 .2.6900 .2300E-12 .1.5000 .0000E-00 .0000 .0000
.0710 .100.00 .1700E-05 .1200 .0000E+00 .0000 .3000E+11 .0000 .1200E-03 .1.0000 .0000
.3120 .50 .0000E+11 .0000 .0000E+00 .0000 .1000E-03 .2.4000 .0000E-00 .0000 .0000
.3120 .15.00 .0000E+11 .0000 .0000E+00 .0000 .1400E-03 .1.7000 .0000E-00 .0000 .0000
.3060 .50 .6100E-04 .0000 .0000E+00 .0000 .1400E-04 .2.2700 .0000E-00 .0000 .0000
.3060 .40.00 .6100E-04 .0000 .0000E+00 .0000 .1400E-04 .2.4000 .0000E-00 .0000 .0000

INITIAL CURRENT= 10000.00 UNIT. BRCD. 3.- .0550 GAMMA .60 1. EXTCTN=3000000.00 CMTI INT. .0140

INIT. VELOCITY= .5710.33 UNIT CSD. AREA = .188900 INITIAL TEMPERATURE = 4.5000
ALPHA = .00500 INTR. X VELOCITY= .355.4250 REFLECTON= .76000 INTR. Y VELOCITY= 4601.6300
X CMTI DIMENSION= 8.00 Y CMTI DIMENSION= 1.14 Z CMTI DIMENSION= 172.30
COORDINATES OF SOURCE Y= 1.00 Y= .60 Z = 56.20
DECELER DELAY TIME = 50 INITIAL MAGNETIC FIELD= 117.600Kga

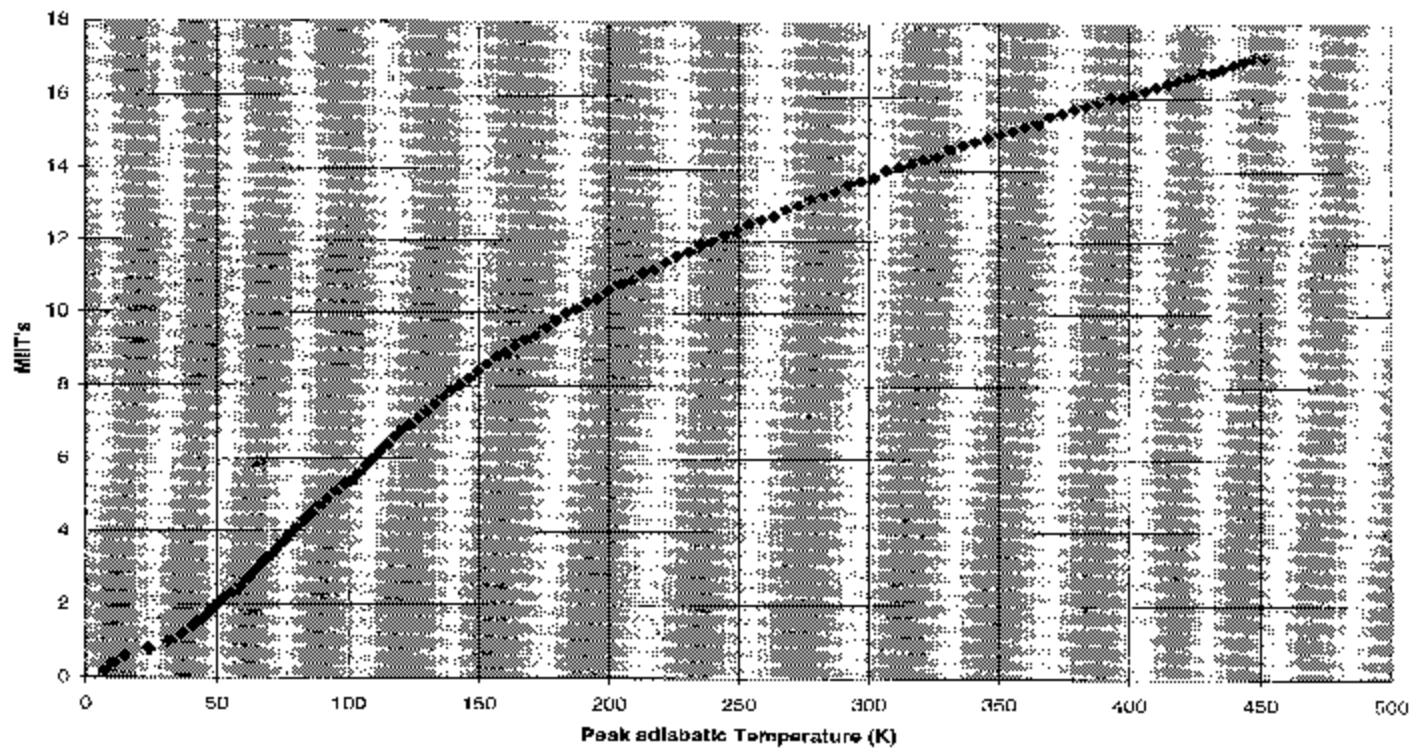
TIME CURRENT CMTI ELECTRIC FIELD VOLTAGE RMT. VOLTAGE LND ENERGY INT. VOLTAGE ALPHA LOGP
.001000, 9999.99, .435099E-04, .0250323402, 0, 2.36, 44, 5.11, -.
.002000, 9999.92, .030326E-04, .1040623402, 0, 3.30, 97, 7.15, 2.
.003000, 9999.93, .175516E-03, .1744353402, 0, 17.55, 76, 8.93, 3.
.004000, 9999.66, .201250E-03, .3743073102, 0, 20.12, 2.92, 11.42, 4.
.005000, 9999.40, .441756E-03, .3150733102, 0, 44.10, 4.13, 10.16, 5.
.006000, 9999.07, .626956E-03, .3057333102, 0, 62.62, 6.30, 24.36, 6.
.007000, 9999.00, .651754E-03, .4554033402, 0, 65.10, 9.52, 29.22, 7.
.008000, 9997.99, .111453E-02, .523103402, 0, 111.42, 12.14, 31.27, 8.
.009000, 9997.10, .111750E-02, .592935E+02, 0, 141.72, 14.17, 33.82, 9.
.010000, 9997.33, .175153E-02, .571409E+02, 0, 172.00, 17.22, 36.04, 1.7.
.011000, 9998.10, .204250E-02, .596754E+02, 0, 204.05, 20.42, 38.02, 1.1.
.012000, 9998.76, .238897E-02, .610753E+02, 0, 238.39, 23.95, 39.97, 1.2.
.013000, 9999.04, .275757E-02, .630010E+02, 0, 275.42, 27.56, 42.47, 1.3.
.014000, 9999.49, .315713E-02, .660594E+02, 0, 315.23, 31.55, 42.99, 1.4.
.015000, 9998.60, .357551E-02, .699753E+02, 0, 357.30, 35.76, 42.47, 1.5.
.016000, 9998.30, .397524E-02, .809382E+02, 0, 397.07, 39.75, 45.02, 1.6.
.017000, 9999.89, .427814E-02, .876431E+02, 0, 435.87, 43.73, 47.35, 1.7.
.018000, 9998.21, .478269E-02, .997000E+02, 0, 478.65, 47.76, 49.75, 1.8.
.019000, 9978.32, .519945E-02, .948855E+02, 0, 517.39, 51.90, 50.14, 1.9.
.020000, 9970.21, .562637E-02, .937369E+02, 0, 560.76, 56.17, 51.30, 2.0.
.021000, 9971.30, .606441E-02, .978973E+02, 0, 603.47, 60.49, 53.85, 2.1.
.022000, 9968.24, .651446E-02, .970766E+02, 0, 647.78, 64.96, 57.10, 2.2.
.023000, 9964.38, .697023E-02, .916571E+02, 0, 693.31, 69.35, 55.72, 2.3.
.024000, 9960.25, .744075E-02, .913571E+02, 0, 740.59, 74.37, 56.95, 2.4.
.025000, 9956.88, .794461E-02, .908988E+02, 0, 788.14, 79.13, 59.16, 2.5.
.026000, 9951.18, .845083E-02, .908032E+02, 0, 837.59, 84.13, 57.07, 2.6.
.027000, 9946.77, .897261E-02, .905364E+02, 0, 888.51, 89.20, 50.78, 2.7.
.028000, 9940.57, .951138E-02, .901374E+02, 0, 940.32, 94.60, 52.00, 2.8.
.029000, 9935.41, .1.00675E-01, .893432E+02, 0, 994.60, 100.09, 53.48, 2.9.
.030000, 9929.53, .1.06401E-01, .87546E+02, 0, 1050.51, 102.70, 54.69, 3.0.

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RD- 3 outer winding cable Miit's Curve

RD3 outer Coil Miit's vrs Peak Temperature





Protection of D20

A very conservative approach was taken:

70% of the magnet was under heaters

The power levels were for SF operation

Layer 1 = 53 watts/cm²

Layer 2 = 23 “

Layer 3 = 29 “

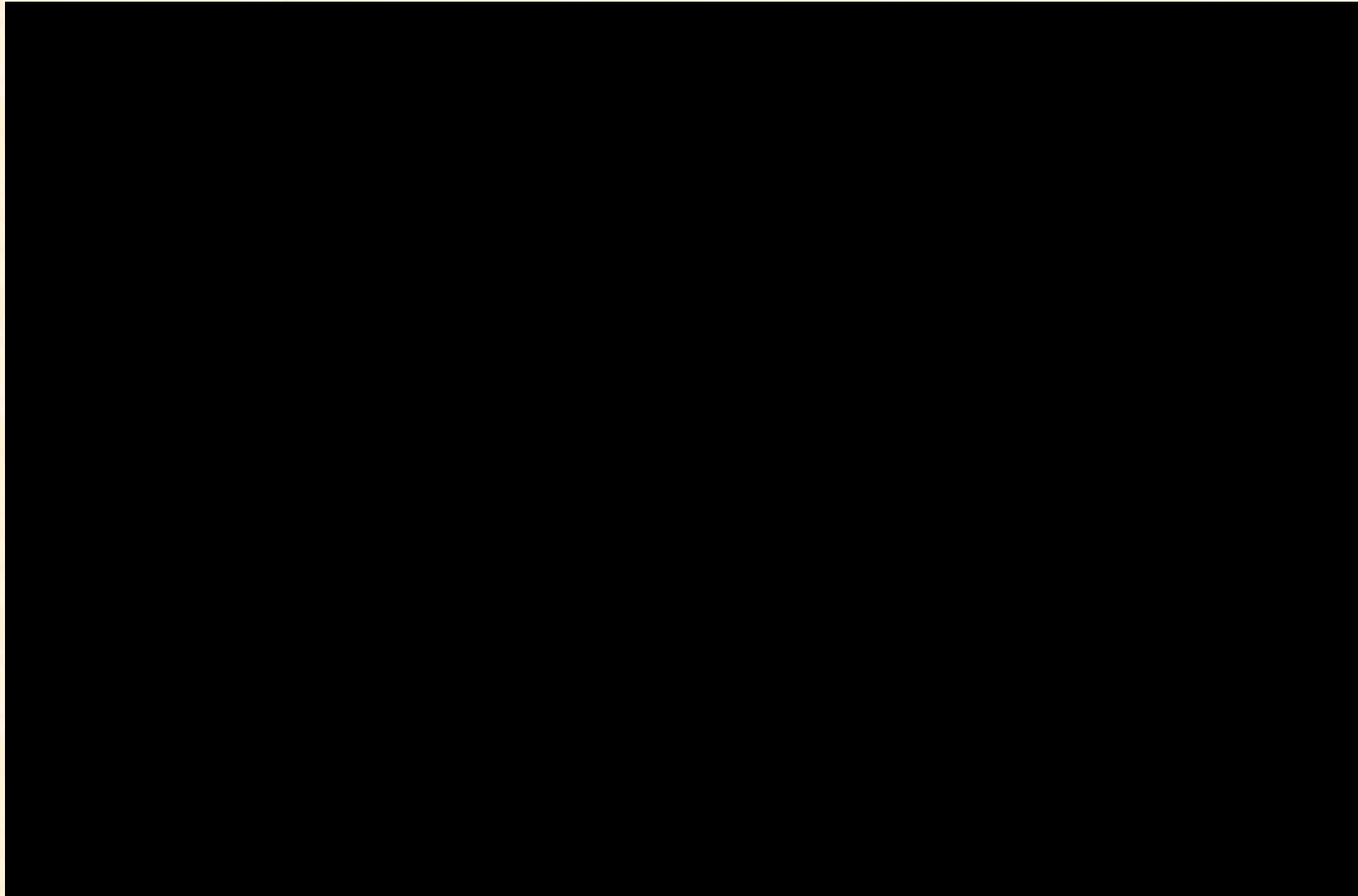
Layer 4 = 27 “

The data for Quench was:

The Miit's Curve:



Miit's Curves for C0/D0 Quads, Tev, & D20





Integrated Stainless Steel Specific Heat versus Peak Temperature

Table

| Temperature Adiabatic(K) | Energy/unit volume joules/cubic centimeter |
|---------------------------------------|--|
| 100 | 80 |
| 200 | 316 |
| 300 | 642 |
| 400 | 1034 |
| 500 | 1494 |
| Kapton Failure | 770 |
| 2700 | |
| Typical Resistivity (Stainless Steel) | 50 micro-ohm-cm |
| RRR | 1.5 |
| Typical Time constants (1/e) | |
| Heater pulse | 30 – 10 milliseconds |
| Typical detection plus thermal | |
| Diffusion time at 70% short Sample | 40 milliseconds |
| (typical peak Miit value) | |
| Typical heater Power supply | 450v |
| Parameters (x2 if stacked) | 2 to 20 millifarad |



Summary of typical process

| | |
|---|--|
| Obtain Miits curve for magnet | Calculate from “Quench” code or Measure the 450K point |
| Calculate minimum coil volume | I (operate), L (millihenries) |
| Design heater area greater than that to switch min. coil vol. | Heater area calculated |
| Heater design resistances calculated | ohms to few 10’s of ohms |
| Temperature (heater) targets | 150K to 200K |
| Wattage (heater) at the surface | $\geq 20\text{w/ cm}^2$ for LHe & ≥ 40 for SFHe |
| Time (heater) constants | 30 millisec. to ≤ 100 millisec. |

An efficient heater should:

| | |
|--|--|
| Include an active length (non-cu plated) | ≥ 1 cable transposition length |
| Minimum heater thickness (ss) | 13 micron preferred, but 25 micron is normal |
| Min. thickness Kapton under layer and/ or Alumna filled Kapton (x2 thermal conduct.) | 15 microns (≥ 3 kV checked) “ 3kV? |

Can include diagnostic wiring traces